## IN THE CLAIMS

Please amend the claims as follows:

## 1. (Cancelled)

- 2. (Previously Presented) An optical scanning device for scanning optical record carriers with radiation of a selected wavelength, the device including an objective lens, having an axial direction and a radial direction, the objective lens having a phase structure which is non-periodic with respect to the radial direction, the non-periodic phase structure being arranged to compensate for comatic aberrations generated in the objective lens when an optical record carrier is read in a direction which is non-axial with respect to said objective lens, wherein said non-periodic phase structure compensates at least 50% of the root mean square (rms) comatic wavefront error at a certain field angle with respect to the axial direction and caused by the objective.
- 3. (Previously Presented) The optical scanning device of claim 2, wherein said non-periodic phase structure compensates at least 70% of the root mean square (rms) comatic wavefront error at said certain field angle.
- 4. (Previously Presented) An optical scanning device for scanning optical record carriers with radiation of a selected wavelength, the device including an objective lens, having an axial direction and a radial direction, the objective lens

having a phase structure which is non-periodic with respect to the radial direction, the non-periodic phase structure being arranged to compensate for comatic aberrations generated in the objective lens when an optical record carrier is read in a direction which is non-axial with respect to said objective lens, wherein the rms wavefront error caused by the comatic aberration generated by the objective lens at a maximum required field angle with respect to the axial direction, as compensated by the non-periodic phase structure, is less than 40ml.

- 5. (Previously Presented) The optical scanning device of claim
- 4, wherein the rms wavefront error is less than  $20m\lambda$ .
- 6. (Previously Presented) An optical scanning device for scanning optical record carriers with radiation of a selected wavelength, the device including an objective lens, having an axial direction and a radial direction, the objective lens having a phase structure which is non-periodic with respect to the radial direction, the non-periodic phase structure being arranged to compensate for comatic aberrations generated in the objective lens when an optical record carrier is read in a direction which is non-axial with respect to said objective lens, wherein said non-periodic phase structure includes a plurality of annular zones, each of said zones comprising a step of a substantially constant height with respect to a rotationally symmetrical aspheric shape generally followed by said objective lens, said step having a surface located at the substantially constant height such that all points on said step surface are located at about a constant distance from said aspheric shape.

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- 7. (Previously Presented) The optical scanning device of claim 6, wherein said steps generate a relative phase difference of approximately a multiple of  $2\pi$  for radiation of said selected wavelength when an optical record carrier is read in said axial direction.
- 8. (Previously Presented) The optical scanning device of claim 6, wherein the radial widths of said zones are selected in dependence on the comatic aberration to be compensated for.
- 9. (Previously Presented) The optical scanning device of claim 8, wherein said zones comprise a zone (a) with a nonzero height, measured in relation to said aspheric shape, located in the region in which the normalized pupil coordinate p ranges from 0.45 to 0.84.
- 10. (Previously Presented) The optical scanning device of claim 9, wherein said zone (a) ends prior to a normalized pupil coordinate p of 0.85.
- 11. (Previously Presented) The optical scanning device of claim 8, wherein said zones comprise a zone (b) with a nonzero height, measured in relation to said aspheric shape, located in the region in which the normalized pupil coordinate r ranges from 0.9 to 1.00.
- 12. (Previously Presented) The optical scanning device of claim 11, wherein said zones comprise a plurality of zones with a

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nonzero height, measured in relation to said aspheric shape, located in the region in which the normalized pupil coordinate  $\rho$  ranges from 0.9 to 1.00.

- 13. (Previously Presented) The optical scanning device of claim 6, wherein the heights of said zones are selected substantially optimally in relation to the comatic aberration to be compensated for.
- 14. (Previously Presented) The optical scanning device of claim 7, wherein the number of said zones is greater than four.
- 15. (Previously Presented) The optical scanning device of claim 8, wherein the number of said zones is less than ten.
- 16. (Previously Presented) The optical scanning device of claim 9, wherein said non-periodic phase structure is formed on the surface of said objective lens.
- 17. (Previously Presented) An optical system including an optical element having optical power and an axial direction and a radial direction, the optical element having a phase structure which is non-periodic with respect to the radial direction, the non-periodic phase structure being arranged to compensate for comatic aberrations generated by the optical element when an optical beam traverses the optical system in a direction which is non-axial with respect to said element, the non-periodic phase structure having a first step, the first step having a surface located opposite to a surface shape followed by the

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optical element such that all points on the surface of the first step are located at about a constant distance from said surface shape.

- 18. (Currently Amended) The optical system of claim 18 17, wherein the surface of the first step is oriented substantially parallel to said surface portion.
- 19. (Currently Amended) The optical seaming system device of claim  $\frac{18}{17}$ , wherein the non-periodic phase structure comprises a plurality of steps that includes the first step, and wherein said steps generate a relative phase difference of approximately a multiple of  $2\pi$  when said optical beam is directed in said axial direction.
- 20. (Currently Amended) The optical seanning system device of claim 18 17, wherein said non-periodic phase structure compensates at least 50% of the root mean square (rms) comatic wavefront error at a certain field angle with respect to the axial direction and caused by the optical element.
- 21. (Currently Amended) The optical scanning system device of claim 18 17, wherein the rms wavefront error caused by the comatic aberration generated by the optical element at a maximum required field angle with respect to the axial direction, as compensated by the non-periodic phase structure, is less than 40ml.

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- 22. (Currently Amended) The optical scanning device system of claim 18 17, wherein said surface shape comprises an aspheric shape.
- 23. (Currently Amended) The optical system scanning device of claim 6, wherein the step surface is oriented substantially parallel to said aspheric shape.